

Analysis and Design of Analog Integrated Circuits
Lecture 16

Subthreshold Operation and g_m/I_d Design

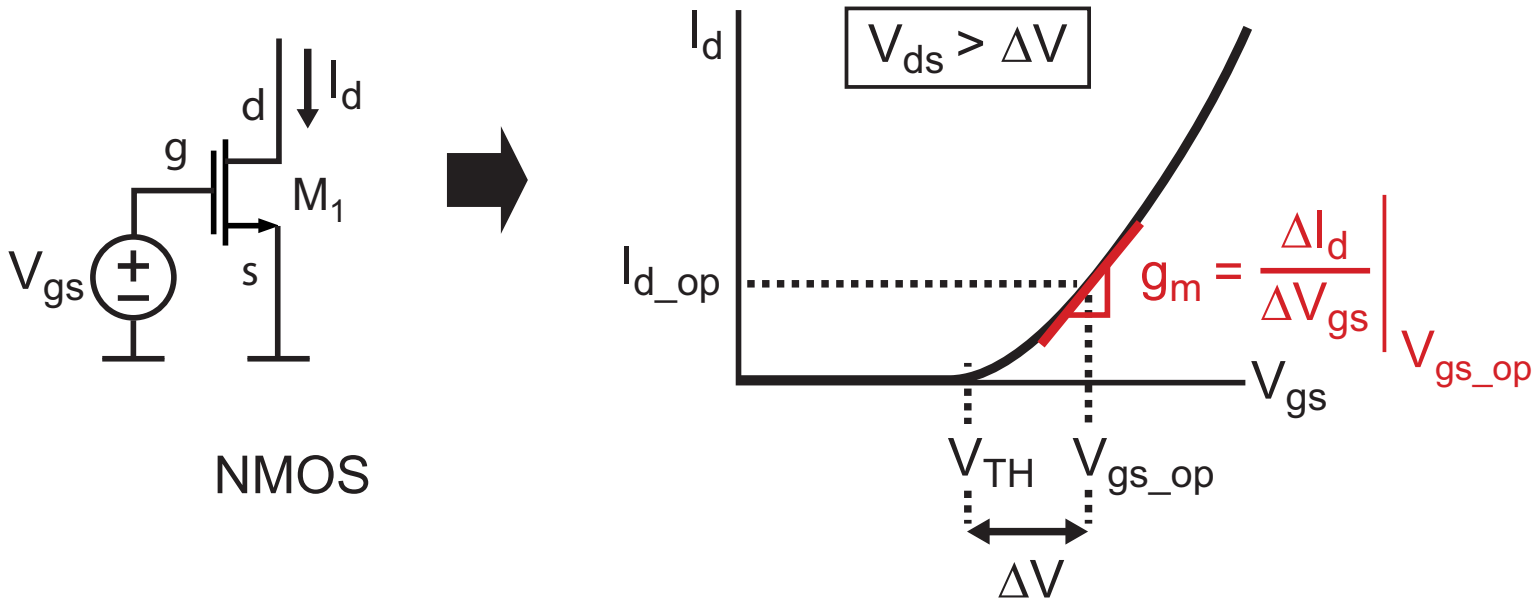
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A Closer Look at Transconductance



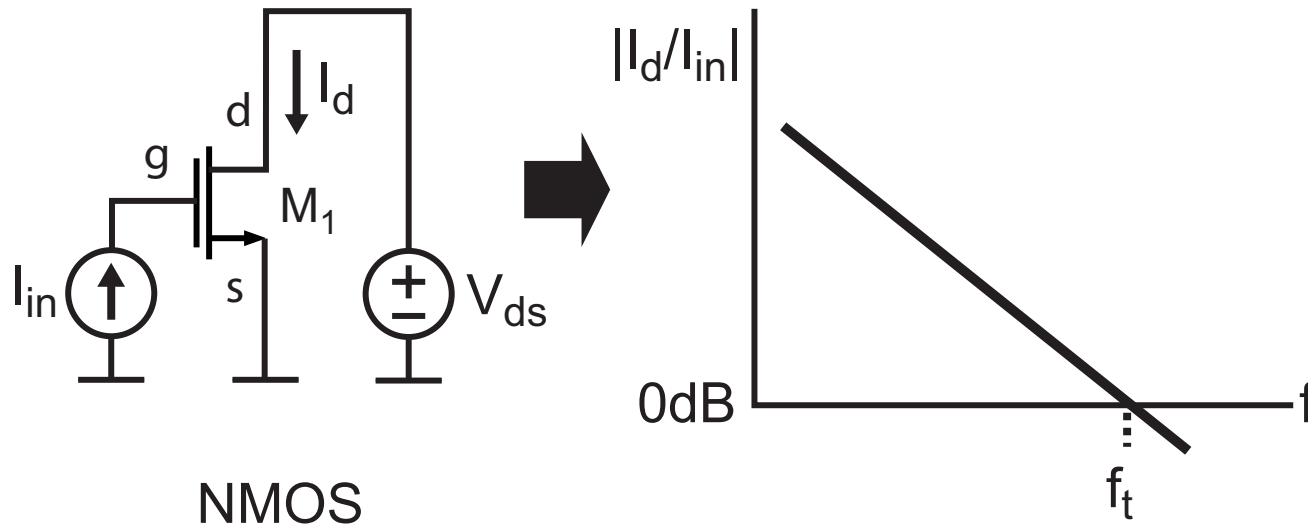
- Assuming device is in strong inversion and in saturation:

$$I_D = \frac{\mu_n C_{ox} W}{2 L} (V_{gs} - V_{TH})^2 (1 + \lambda V_{ds})$$

$$\Rightarrow g_m = \frac{\delta I_d}{\delta V_{gs}} \approx \mu_n C_{ox} \frac{W}{L} (V_{gs} - V_{TH}) \approx \sqrt{2 \mu_n C_{ox} \frac{W}{L} I_d}$$

$$\Rightarrow g_m \approx \frac{I_d \sqrt{2 \mu_n C_{ox} W / L}}{\sqrt{I_d}} \approx \frac{2 I_d}{(V_{gs} - V_{TH})}$$

Unity Gain Frequency for Current Gain, f_t



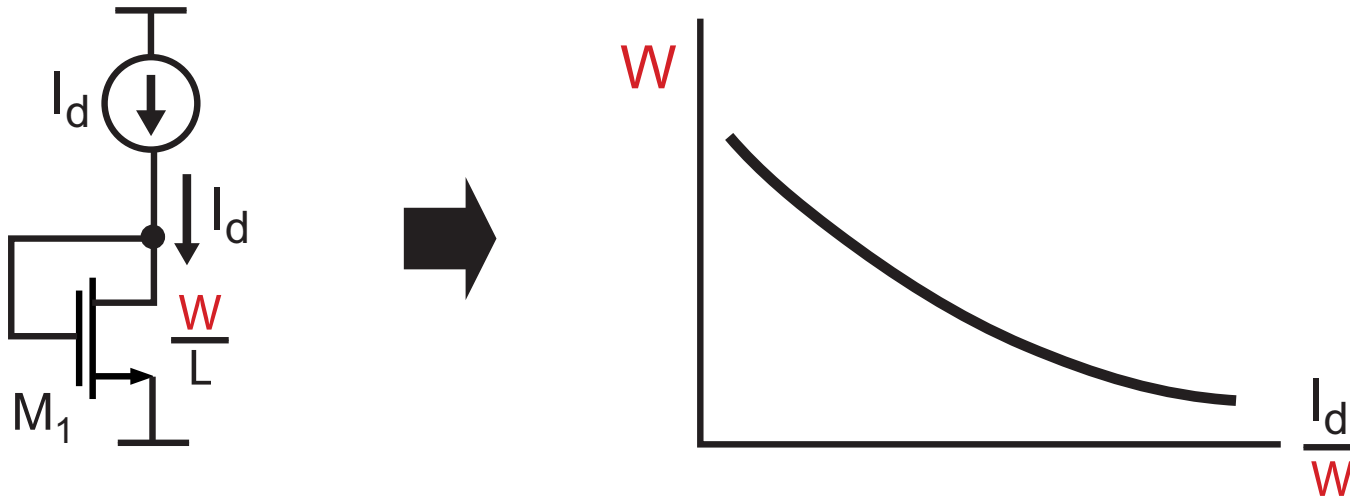
- Under fairly general conditions, we calculate:

$$I_d(s) \approx I_{in}(s) \frac{1}{s(C_{gs} + C_{gd})} g_m \quad \Rightarrow \quad \frac{I_d(s)}{I_{in}(s)} \approx \frac{g_m}{s(C_{gs} + C_{gd})}$$

$$\Rightarrow \boxed{f_t = \frac{g_m}{2\pi(C_{gs} + C_{gd})}}$$

- f_t is a key parameter for characterizing the achievable gain-bandwidth product with circuits that use the device

Current Density as a Key Parameter



- **Current density is defined as the ratio I_d/W :**
 - We'll assume that current density is altered by keeping I_d fixed such that only W varies
 - Maintains constant power
 - r_o (i.e., $1/g_{ds} = 1/(\lambda I_d)$) will remain somewhat constant

Investigating Impact of Current Density

- For simplicity, let us assume that the CMOS device follows the square law relationship

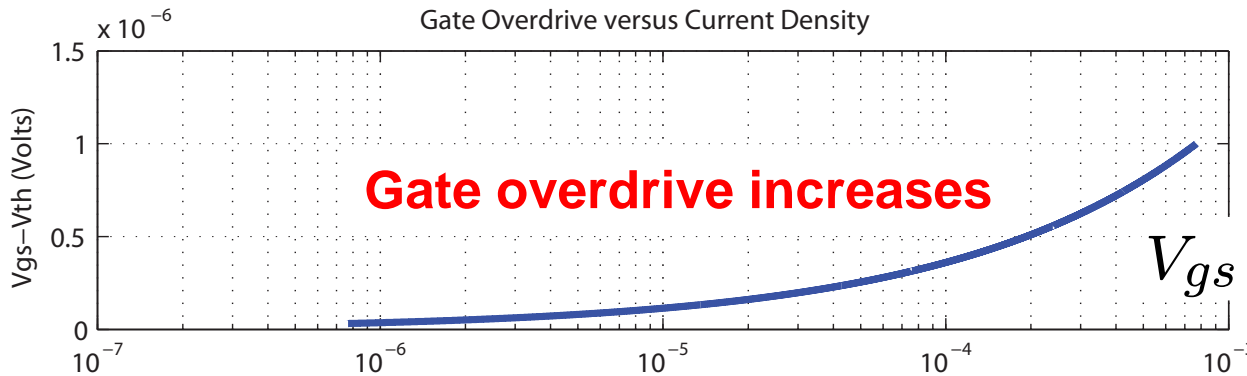
$$I_D \approx \frac{\mu_n C_{ox} W}{2L} (V_{gs} - V_{TH})^2$$

- This will lead to the formulations:

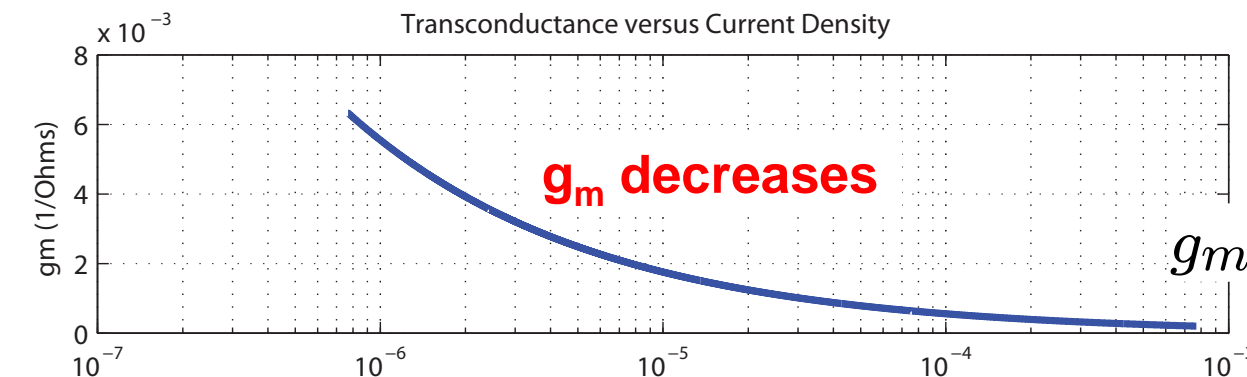
$$V_{gs} - V_{TH} \approx \sqrt{\frac{2L}{\mu_n C_{ox}} \left(\frac{I_d}{W} \right)} \quad g_m \approx \frac{2I_d}{V_{gs} - V_{TH}}$$

- These formulations are only accurate over a narrow region of strong inversion (with the device in saturation)
- However, the general trends observed from the above expressions as a function of current density will provide useful insight

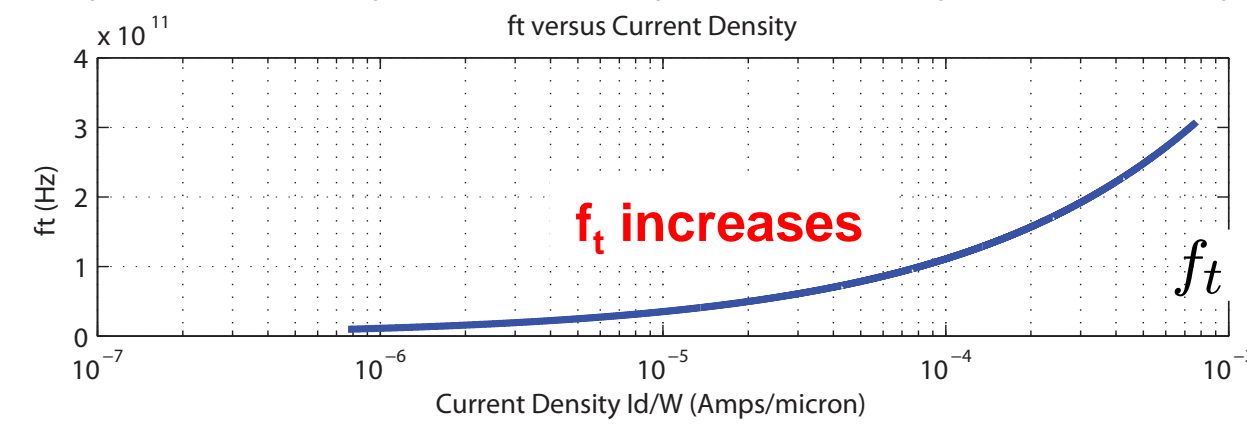
Investigate the Impact of Increasing Current Density



$$V_{gs} - V_{TH} \approx \sqrt{\frac{2L}{\mu_n C_{ox}} \left(\frac{I_d}{W} \right)}$$



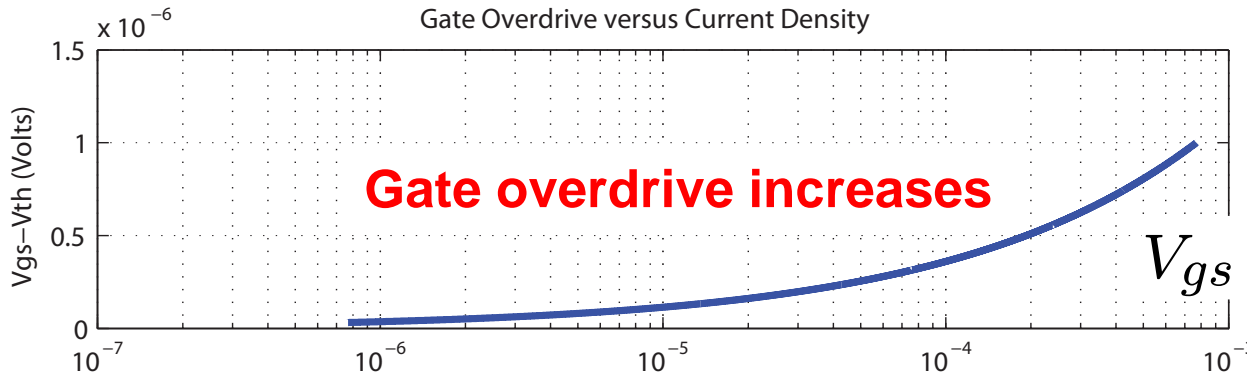
$$g_m \approx \frac{2I_d}{V_{gs} - V_{TH}}$$



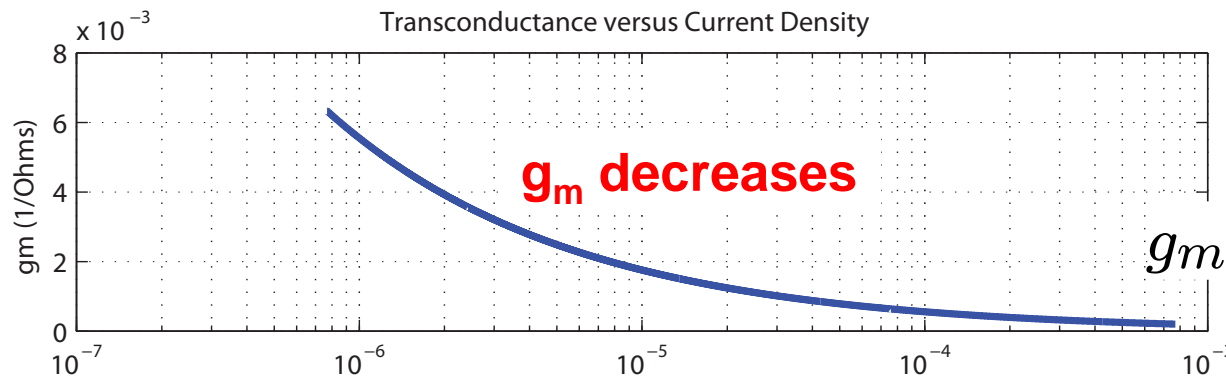
$$f_t = \frac{1}{2\pi C_{gs}} g_m \propto \frac{\sqrt{W}}{W}$$

W decreased with fixed I_d

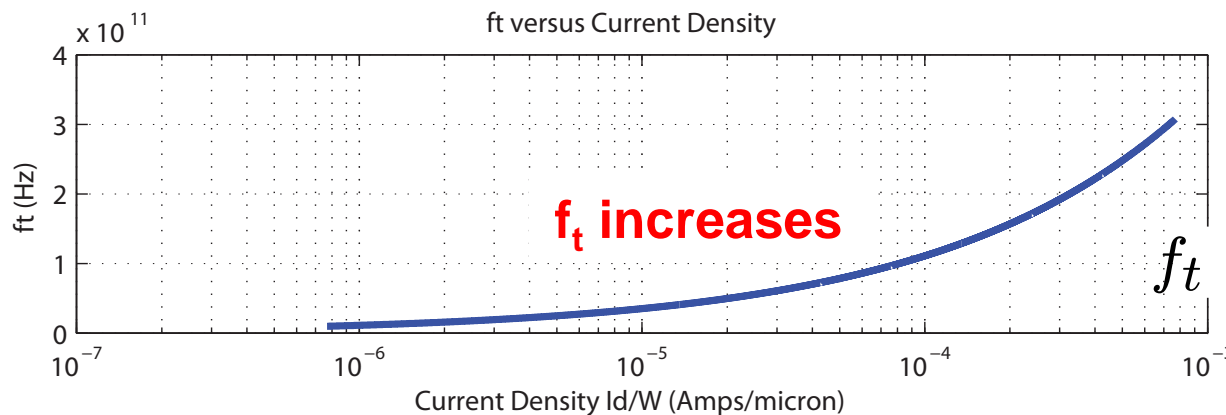
Transconductance Efficiency Versus f_t



$$V_{gs} - V_{TH} \approx \sqrt{\frac{2L}{\mu_n C_{ox}} \left(\frac{I_d}{W} \right)}$$



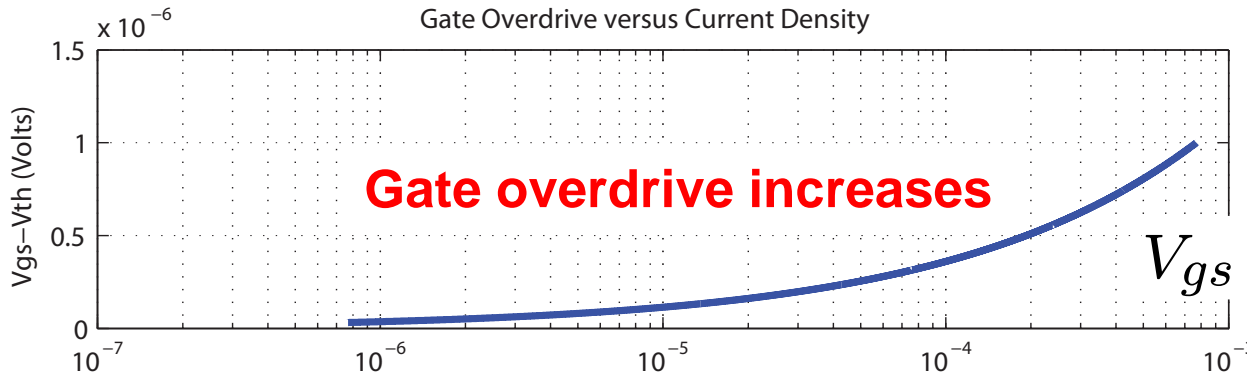
$$g_m \approx \frac{2I_d}{V_{gs} - V_{TH}}$$



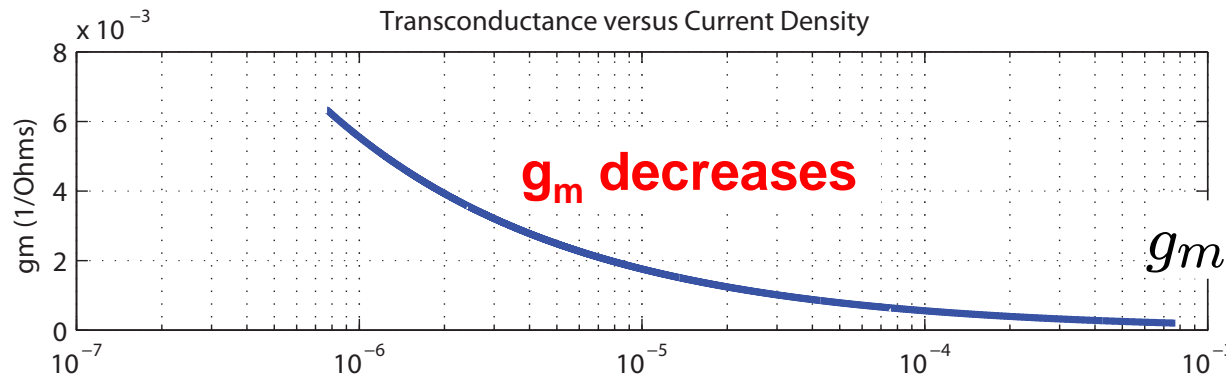
$$f_t = \frac{1}{2\pi C_{gs}} g_m \propto \frac{\sqrt{W}}{W}$$

Higher g_m (more gain) \leftarrow \rightarrow Higher f_t (faster speed)

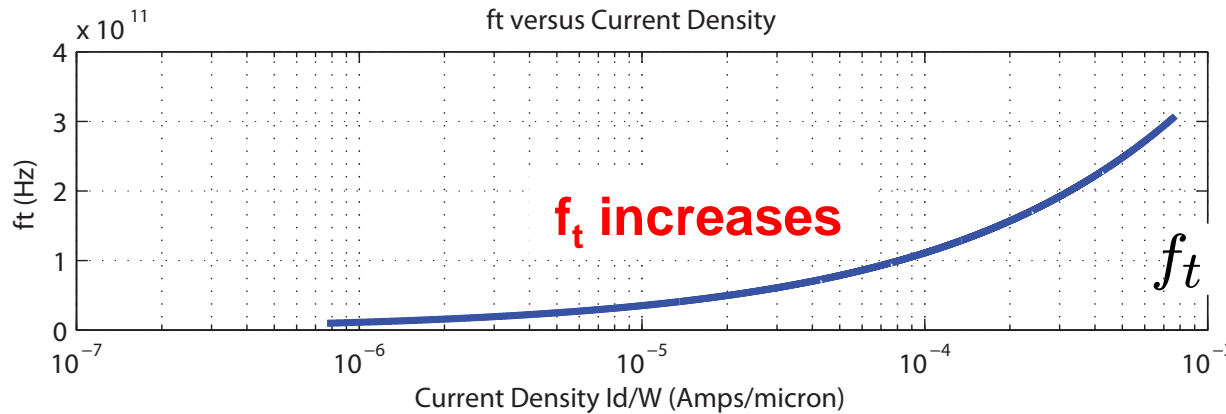
Transistor "Inversion" Operating Regions



$$V_{gs} - V_{TH} \approx \sqrt{\frac{2L}{\mu_n C_{ox}} \left(\frac{I_d}{W} \right)}$$



$$g_m \approx \frac{2I_d}{V_{gs} - V_{TH}}$$



$$f_t = \frac{1}{2\pi C_{gs}} g_m \propto \frac{\sqrt{W}}{W}$$

Weak Moderate Strong

Key Insights Related to Current Density

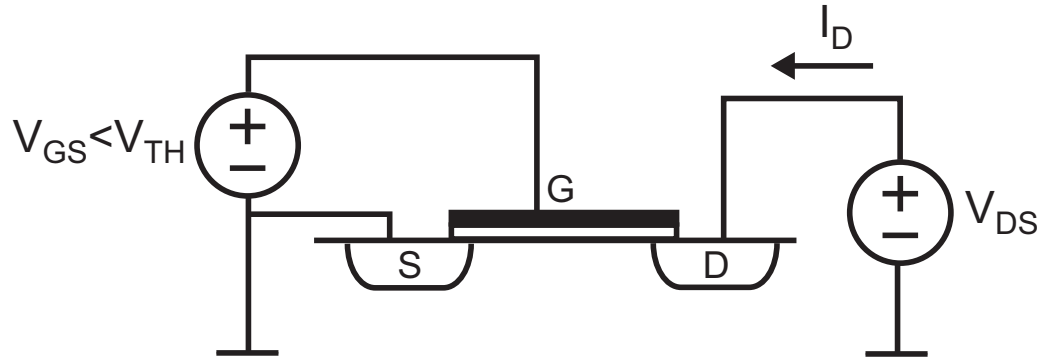
- **Current density sets the device operating mode**
 - **Weak inversion (subthreshold): highest g_m efficiency**
 - Achieves highest g_m for a given amount of current, I_d
 - **Strong inversion: highest f_t**
 - Achieves highest speed for a given amount of current, I_d
 - **Moderate inversion: compromise between the two**
 - Often the best choice for circuits that do not demand the highest speed but cannot afford the low speed of weak inversion (subthreshold operation)

- **Key issue: validity of square law current assumption**

$$I_D = \frac{\mu_n C_{ox} W}{2 L} (V_{gs} - V_{TH})^2 (1 + \lambda V_{ds})$$

- **The above is only accurate over a narrow range of strong inversion (i.e., the previous plots are inaccurate)**
 - General observations above are still true, though

A Proper Model for Subthreshold Operation



- **Drain current:**

$$I_D = I_{D0} \frac{W}{L} e^{V_{gs}/(nV_t)} (1 - e^{-V_{ds}/V_t})$$

- **Where:**

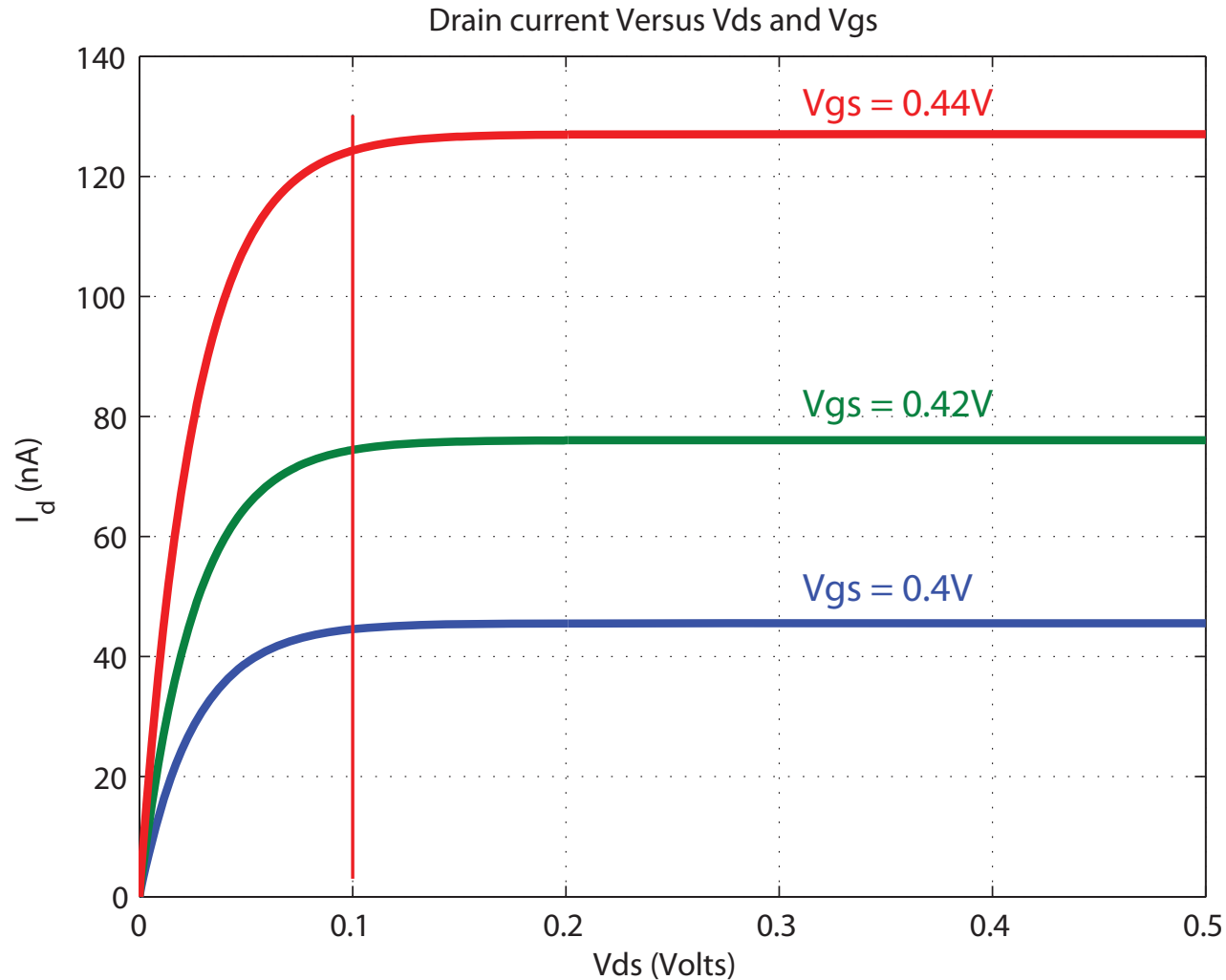
$$V_t = \frac{kT}{q} \approx 26\text{mV at } T = 300\text{K}$$

$$n = \frac{C_{ox} + C_{depl}}{C_{ox}} \approx 1.5$$

$$I_{D0} = \mu_n C_{ox} (n - 1) V_t^2 e^{-V_{TH}/(nV_t)}$$

- **Note: channel length modulation, i.e., λ , is ignored here**

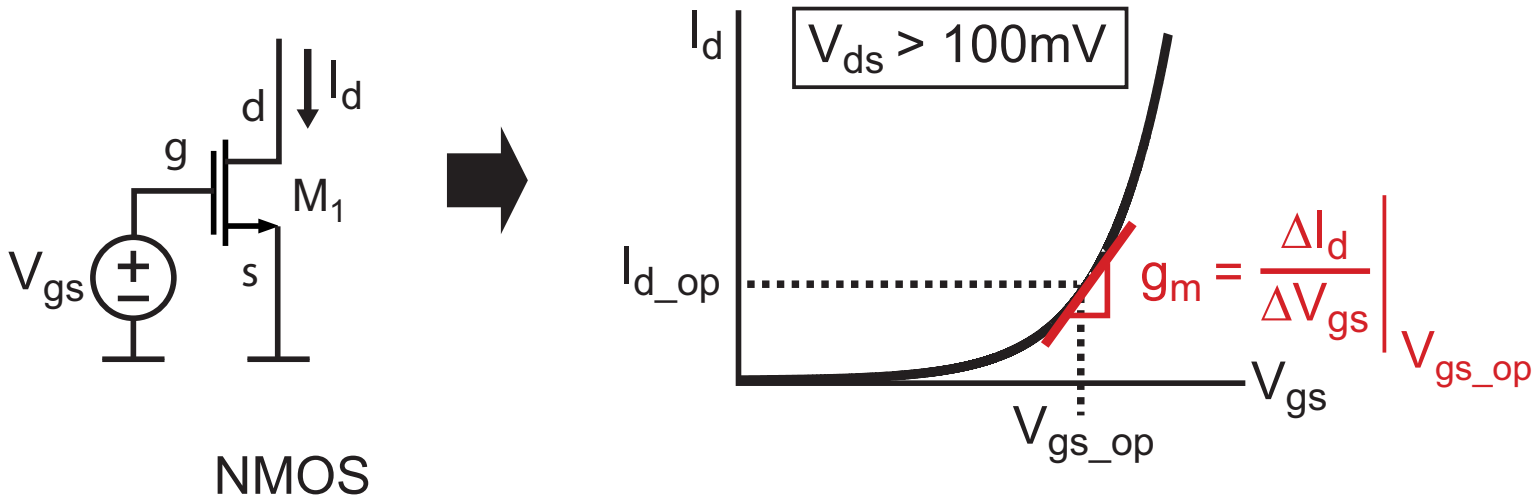
Saturation Region for Subthreshold Operation



- **Saturation occurs at roughly $V_{ds} > 100$ mV**

$$\Rightarrow I_D = I_{D0} \frac{W}{L} e^{V_{gs}/(nV_t)} \left(1 - e^{-V_{ds}/V_t} \right) \approx I_{D0} \frac{W}{L} e^{V_{gs}/(nV_t)}$$

Transconductance in Subthreshold Region



- Assuming device is in subthreshold and in saturation:

$$I_D \approx I_{D0} \frac{W}{L} e^{V_{gs}/(nV_t)}$$

g_m purely a function of I_d !

$$\Rightarrow g_m = \frac{\delta I_d}{\delta V_{gs}} \approx I_{D0} \frac{W}{L} e^{V_{gs}/(nV_t)} \frac{1}{nV_t} = \boxed{\frac{I_d}{nV_t}}$$

Recall for strong inversion : $g_m \approx \boxed{\frac{2I_d}{(V_{gs} - V_{TH})}}$

Comparison of Strong and Weak Inversion for g_m

- Assumption: I_d is constant with only W varying
- Strong inversion formulation predicts ever increasing g_m with reduced overdrive voltage

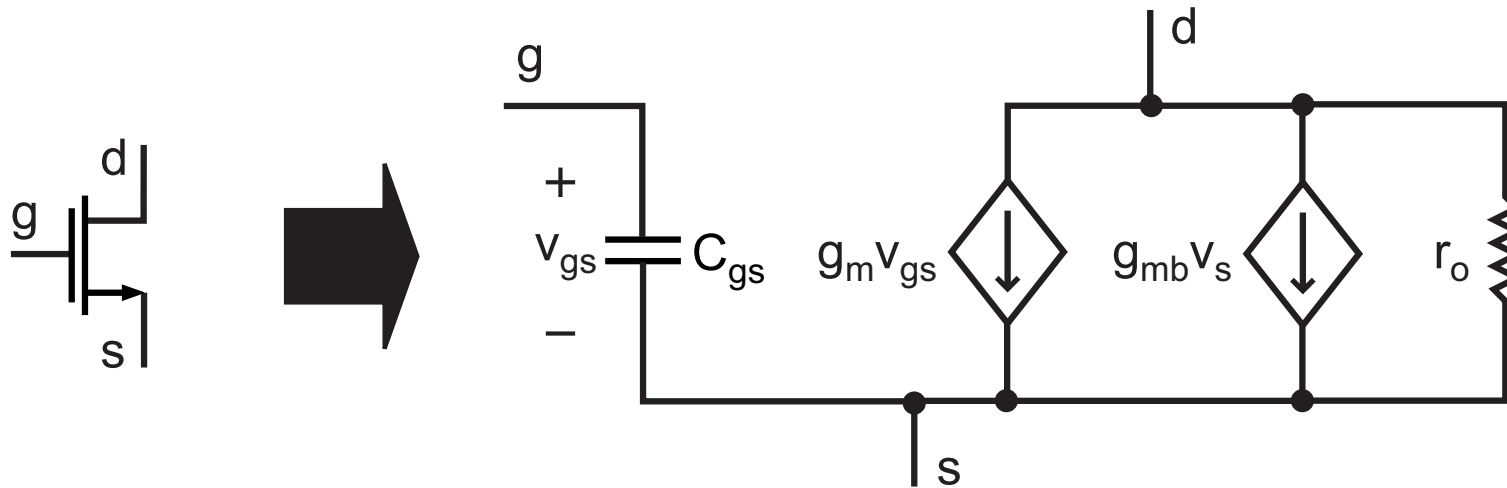
$$g_m \approx \frac{2I_d}{(V_{gs} - V_{TH})}$$

- Reduced current density leads to reduced overdrive voltage and therefore higher g_m
- Weak inversion formulation predicts that g_m will hit a maximum value as current density is reduced

$$g_m \approx \frac{I_d}{nV_t}$$

- Note that the area of the device no longer influences g_m when operating in weak inversion (i.e., subthreshold)

Hybrid- π Model in Subthreshold Region (In Saturation)

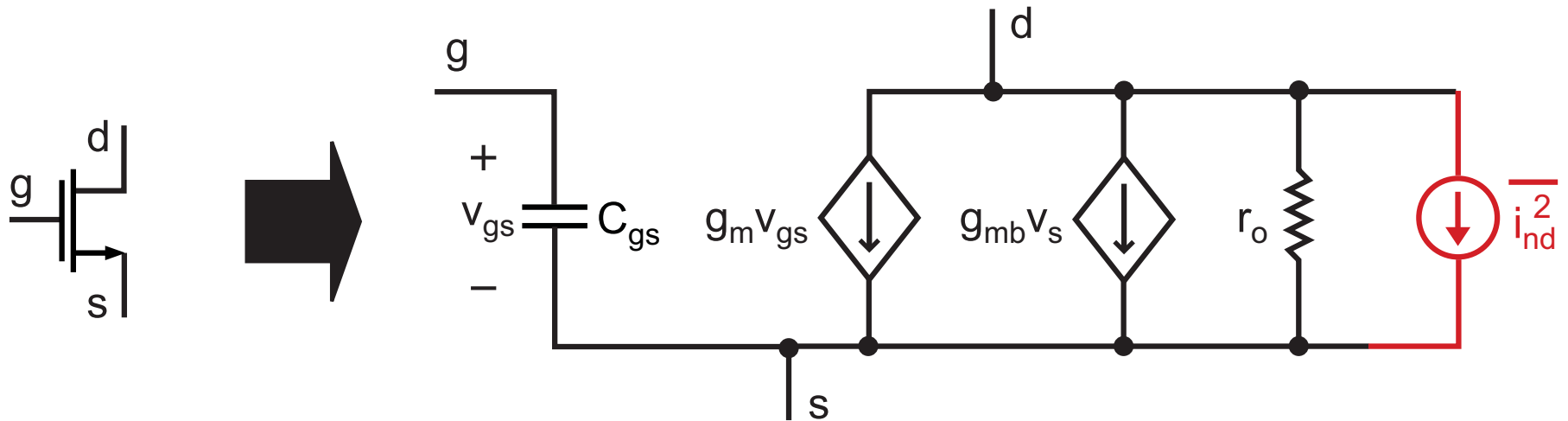


- Looks the same in form as for strong inversion, but different expressions for the various parameters

$$g_m \approx \left(\frac{1}{n}\right) \frac{I_d}{V_t} \quad g_{mb} \approx \left(\frac{n-1}{n}\right) \frac{I_d}{V_t} \quad r_o \approx \frac{1}{\lambda I_d}$$

- We can use the very same Thevenin modeling approach as in strong inversion
 - We just need to calculate g_m and g_{mb} differently

Noise for Subthreshold Operation (In Saturation)



- Recall transistor drain noise in strong inversion:

$$\overline{i_{nd}^2} = \underbrace{4kT\gamma g_{dso}\Delta f}_{\text{Thermal noise}} + \underbrace{\frac{K_f}{f} \frac{g_m^2}{WLC_{ox}^2}\Delta f}_{\text{1/f noise}}$$

- In weak inversion (i.e., subthreshold):

$$\overline{i_{nd}^2} = \underbrace{2kTng_m\Delta f}_{\text{Thermal noise}} + \underbrace{\frac{K_f}{f} \frac{g_m^2}{WLC_{ox}^2}\Delta f}_{\text{1/f noise}}$$

Strong Inversion Versus Weak Inversion

- **Strong inversion ($V_{gs} > V_{TH}$)**

- Poor g_m efficiency (i.e., g_m/I_d is low) but fast speed
- Need $V_{ds} > (V_{gs} - V_{TH}) = \Delta V$ to be in saturation
- Key device parameters are calculated as:

$$g_m \approx \frac{2I_d}{(V_{gs} - V_{TH})} \quad g_{mb} \approx \frac{\gamma g_m}{2\sqrt{2|\Phi_F| + V_{SB}}} \quad r_o \approx \frac{1}{\lambda I_d}$$

- **Weak inversion ($V_{gs} < V_{TH}$)**

- Good g_m efficiency (i.e., g_m/I_d is high) but slow speed
- Need $V_{ds} > 100\text{mV}$ to be in saturation
- Key device parameters are calculated as:

$$g_m \approx \left(\frac{1}{n}\right) \frac{I_d}{V_t} \quad g_{mb} \approx \left(\frac{n-1}{n}\right) \frac{I_d}{V_t} \quad r_o \approx \frac{1}{\lambda I_d}$$

- **Moderate inversion: compromise between the two**

Thevenin Modeling Techniques Can Be Applied to All Cases

g_m/I_d Design

- g_m/I_d design is completely SPICE based
 - Hand calculations of g_m , r_o , etc. are not performed
- Various transistor parameters are plotted in terms of g_m/I_d
 - Low g_m/I_d corresponds to strong inversion
 - High g_m/I_d corresponds to weak inversion
- Once a given value of g_m/I_d is chosen, it constrains the relationship between W , L , f_t , etc. such that the sizing of devices becomes a straightforward exercise

Useful References Related to g_m/I_d Design

- **Prof. Bernhard Boser's Lecture:**
 - B. E. Boser, "Analog Circuit Design with Submicron Transistors," IEEE SSCS Meeting, Santa Clara Valley, May 19, 2005,
<http://www.ewh.ieee.org/r6/scv/ssc/May1905.htm>
- **Prof. Boris Murmann's Course Notes:**
 - https://ccnet.stanford.edu/cgi-bin/course.cgi?cc=ee214&action=handout_view&V_section=general
 - See Slides 45 to 67 in particular
- **Prof. Reid Harrison's paper on a low noise instrument amplifier:**
 - http://www.ece.utah.edu/~harrison/JSSC_Jun_03.pdf

Summary

- **CMOS devices in saturation can be utilized in weak, moderate, or strong inversion**
 - Each region of operation involves different expressions for drain current as a function of V_{gs} and V_{ds}
 - It is best to use SPICE to calculate parameters such as g_m , g_{mb} , r_o due to the complexity of the device model in encompassing these three operating regions
 - g_m/I_d methodology is one such approach
 - Weak inversion offers large g_m/I_d but slow speed, and strong inversion offers fast speed but lower g_m/I_d
 - Moderate inversion offers the best compromise between achieving reasonable g_m/I_d and reasonable speed
- **Thevenin modeling approach is valid for all operating regions once g_m , g_{mb} , and r_o are known**